

Production of Metallic and Ceramic Parts with the Optoform Process

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ABSTRACT

Optoform LLC developed a technology to process paste compositions based upon photo-curable resins and fillers. This new process is called by Optoform LLC : the direct composite manufacturing. At the present time, about ten alpha machines have been sold in USA and Europe to set up a collaboration between material developers, process developers and end users.

This technique is quite flexible and allows the development of very different material for many different applications. Mainly, four categories of material have been developed, namely soft material, hard material, metallic and ceramic material. Both last kinds will be the main purpose of this presentation.

Metal (316L, 17-4 PH, Titanium) or ceramic (Zircon/Silica, alumina, hydroxyapatite) powders form about 60 % (in volume) of a pasty photo-curable material.

After the building of the prototype on the Optoform machine, a post-processing is required consisting of a debinding and sintering steps. The debinding consists of removing the resin binder by an appropriate thermal treatment. The debinding parameters are a function of the organic phase and of the powder nature.

After that, the part is sintered in order to produce a full dense part and to enhance the mechanical properties. It is also possible to manage a partial sintering to obtain porous parts which can be used when an auto lubricating is needed.

The bimodal distributions of powder and the particules size will be discussed in relationship with the sintering parameters and with the effect on the mechanical properties.

This new process is a development station for new broad range of rapid prototyping (RP) materials and it represents one more step toward the Rapid Manufacturing of high technical parts.

The Optoform process was well adapted to a broad range of applications for parts as well as for shells or Investment casting cores.

1. INTRODUCTION

Originally, Optoform is a French technology which has been bought by 3D systems in 2001. At the present time, about ten alpha machines have been sold in USA and Europe

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This paper will present the material research and the machine development made by the CRIF and other teams (BCRC, KUL, ENSCI).

This technique is quite flexible and allows the development of very different materials such as soft material, hard material, metallic material (stainless steel 316 L or 17-4PH, titanium...) and ceramic material (Zircon/Silica, Alumina and hydroxyapatite [1]).

One of the main purpose of this conference will be focused on metallic and ceramic materials. Both material kinds require a thermal treatment after processing on Optoform machine. This post-treatment is a debinding and a sintering in order to produce full dense parts or porous ones.

The mechanical properties of the Optoform processed parts are similar to those of parts made by milling.

2. MACHINE PRINCIPLE AND FEATURES

Starting from a 3D file, a part is built on a plateslice by slice from bottom to top. Each succeeding slice is formed by spreading a coating or layer on a plate recovered with a polymer paste which hardens when scanned by a UV laser beam [2]. Figure 1 schematizes the principle of functioning of the Optoform machine.

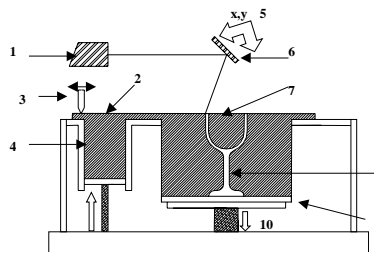


Figure 1 - Optoform principle : 1: UV Laser, 2: Paste supply, 3: recoater including a blade and 2 rotating rods, 4: paste tank, 5: XY rotation, 6: galvanometrical mirror, 7: photosensitive paste, 8: polymerised prototype, 9: building platform, 10: z control.

Because of the scraper stress, supports are needed. The layer thickness is function of the material reactivity to UV and of the application, but it is always in the range of 35 to 120 μ m. The maximum size of the prototype is 250 x 350 x 500 mm but there are also smaller platforms more suitable to process expensive material or to build small prototypes.

Depending on the geometry of the part and on the material, the building speed is about 25 mm/hour and there is no waiting time during the recoating. Unlike usual stereolithography, the UV scanning is immediate after the passage of the blade.

3. MATERIAL DEVELOPMENT

Every material developed for the Optoform machine must comply with some criteria. Each material includes some resin, some fillers (from 20% up to 70% in volume) and a photo-initiator [3]. In addition, the material could contain rheological agent, thixotropic additives and wetting agent.

The paste must have the firmness of a toothpaste which doesn't flow with gravity. The viscosity and the

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flow behaviour of the paste follow the Bingham's model. Thanks to the paste consistency, no vat is needed to build a model.

The paste mixture must be stable with time, and the filler should not deposit sediment, and, the fillers has not to absorb the UV light.

Basic curing resins of those materials are generally acrylates, methacrylates or epoxy [3].

In any case, after building, the parts require a cleaning step. A wise choice of solvent, which will dissolve the paste and not the part, is important to the cleaning step.

Some of those materials produce parts which can be used immediately after processing on the Optoform machine. Such it is the case for soft materials which are used to build gaskets. Hard materials allow the building of:

- Shells for injection of thermoplastic materials like polypropylene random polymer and acrylonitrile butadiene styrene (ABS) in a tool
- Tools realisation for silicon and polyurethane-casting
- Shells for wax injection for investment casting
- Thermoforming tools - Sheet metal forming tools

Metallic and ceramic materials require a thermal post-treatment of debinding and sintering.

4. CERAMIC MATERIAL

Original development of ceramic paste compositions compatible with the Optoform device had been carried out at the SPCTS laboratory (ENSCI-Limoges) [7-8]. Optoform LLC is pursuing the development in this field on his own.

The last two years, CRIF and BCRC have also developed Zircon/Silica and Alumina based formulations. The ceramic concentration in the paste is up to 55 (vol) % [9-10].

The ceramic manufacturing also requires debinding and sintering steps which cause a significant shrinkage needing careful management.

The layer thickness can be in the range of 50 to 100 μ m as a function of the required accuracy in height for the part. The x and y accuracy is limited by the diffraction of the beam due to the ceramic particles. This induces an enlargement of the polymerisation width.

The mechanical properties of Optoform processed ceramic parts are similar valued to those processed using conventional for ceramic processing (pressing).

Some Optoform parts have already been tested as cores in the investment casting process.

CRIF is now developing silicon carbide material. Work to date has employed micron sized particules, but our objective is to develop submicron and perhaps nano-metric, paste material. The debinding and the sintering are performed by INSA of Lyon.

The figure 2 shows greens of small and complex parts (trigger, other mechanism of weapon and a small-scale model of accelerator).



Figure 2: Example of green parts made in SiC

5. METALLIC MATERIAL

Optoform has patented metallic compositions [5-6].

CRIF is also working in collaboration with the KULeuven (Belgium) to develop materials highly filled with metallic powders (60 vol% of metal powder in the paste). The figure 3 shows the homogeneity of the material cured on Optoform. The metallic powder is well dispersed in the photo-curable material. After the building on the Optoform machine, a post-processing is required consisting in debinding and sintering steps. The debinding consists in removing the resin binder by an appropriate thermal treatment. The debinding parameters are a function of the organic phase and of the metallic nature. The most important parameters of debinding are the gas atmosphere (reducing or neutral one), pressure, rate of heating and final temperature.

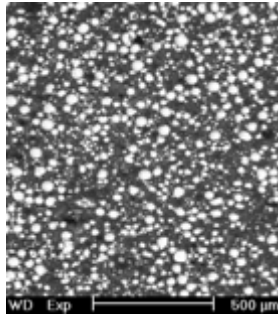


Figure 3. Magnification of 75X. Section in a part cured on Optoform machine. At this step, the part is composed of 60% (Vol) metal and 40% (Vol) resin.

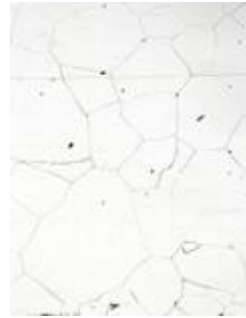


Figure 4. Section in a part of stainless steel after debinding and sintering .

For stainless steel, the residual carbon concentration must be checked. A low residual carbon concentration will induce a sintering at a lower temperature and low mechanical properties (Figure 4). Then, hydrogen atmosphere is not enough efficient to remove all the carbon and to avoid the carbide formation. The following Table 1 illustrates this phenomenon. After the debinding, the sintering is processed in order to produce a full dense metallic part and to enhance the mechanical properties.

Maximum T° of sintering (°C)	Tensile Modulus @ break (MPa)	Elongation @ the break (%)
1360	357	22.5
1380	520	39.9

This is why, CRIF has developed a special binder containing additives which is very efficient in removing organic carbon during debinding. Thanks to those additives the final concentration of carbon is for example about 0.04% for a 316 steel.

It is also possible to manage a partial sintering to obtain porous parts which can be used when auto lubricating is needed or to decrease the shrinkage of massive parts. In this last case, the prototype must be infiltrated with a metal (brass or lower fusion point metal).

Until now, the metallic research was mainly dedicated to the 316L, 17-4PH and Mo-alloys for which the powder selection, the debinding and the sintering has been performed. Some processing trials for Titanium models have been planned.

The trials on stainless steel have demonstrated a bimodal distribution of spherical is more adapted to this process. The average particle diameter can be comprised between 16µm and 60µm.

6 CONCLUSIONS

This new process is more than a new Rapid Prototyping technology. It is a development station for a new broad range of RP materials and it represents one more step toward the Rapid Manufacturing of high

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technical parts.

The Optoform process is well adapted to a broad range of applications for parts as well as for shells.

Materials which can be used directly after Optoform processing or which require post-processing debinding and sintering steps have been developed. The limits or restrictions of use of each type of these materials have been studied in order to meet the requirements and needs of various industrial sectors in the United States and in Europe (e.g. car racing, aerospace and aeronautical sectors, tooling industries, ...).

Despite the expensive investment that an Optoform machine represents, this process is first of all, one more step toward the rapid manufacturing.

REFERENCES

- [1] Industries et Technologies, juin 2004, n°859 – 64-66
- [2] Allanic, A.L.; Schaeffer P. Patent FR2790418-A1 “Procédé de Prototypage permettant l’utilisation de matériau pâteux”
- [3] Kato Yukitoshi et Al. ; Patent WO 00/59972 “Resin composition for photofabrication of three dimensional objects”
- [4] Clarinval, A.-M., Carrus, R. et Dormal, T. Patent pending : 02447249.0 “Photo-polymerisable paste composition”
- [5] Hinczewsky, C.; Patent Fr 2 811 922 – A1 “Composition de pâte chargée de poudre métallique, procédé d’obtention de produits métalliques à partir de ladite composition, et produit métallique obtenu selon ledit procédé
- [6] Khalil M. Moussa et Al., Patent : US 2002/0176793 A1; “Metallic filled pastes
- [7] Hincewsky, C. et Al.; J. Eur. Ceram. Soc., 1998, 18,583-590
- [8] Charlier, T.; Chaput, C.; Doreau, F. Patent WO0042471 “Ceramic Paste Composition and Prototyping Method”
- [9] Delmotte, C.; Erauw, J.P.; Cambier, F.; Carrus, R.; Clarinval, A.M.; Dormal, T. “Shaping II”, Proceedings of the Second International Conference on Saping of Advanced Ceramics (Gent, Belgium, October 24-26, 2002), Luyten, J. and Erauw, J.P. eds, 432-458.
- [10] Delmotte, C.; Erauw, J.P.; Cambier, F. “ECERS”, Proceedings of the Eight Conference & Exhibition of the European Ceramic Society (Istanbul, Turkey, June 29-July 3, 2003), to be published.

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MEETING DISCUSSION – PAPER NO: 14

Author: A. Clarinval

Discusser: Unidentified

Question: 1. Do you have isotropic or anisotropic deformation after debinding? 2. Do you expect to produce an Al part by Optoform?

Response: 1. We observe anisotropic deformation of the part driving the sintering of main parts. The shrinkage is about 16% for metallic parts in three directions. For some geometries with alternating massive-non massive areas, some specific supports must be managed during the sintering to avoid deformation. 2: The melting temperature of Al is too close to the debinding temperatures. A perspective way to obtain light parts will be tested soon: First, the part is built in SiC material on Optoform and then debinded. After that, the part (skeleton) is infiltrated with aluminum.